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CHAPTER 3 ANTENNA ARRAYS AND BEAMFORMING

3.1
$$\sum_{m=1}^M |a_m| e^{j\delta_m} = \sum_{m=1}^M |a_m| e^{j\zeta_m} e^{j\delta_m} \quad (3.2)$$
 Where $|a_m|$ Is The Magnitude And δ_m Is The Phase Of The Weighting Of The m th Element. The Normalized Array Factor Is Given By $F(\theta, \phi) = \sum_{m=1}^M |a_m| e^{j\zeta_m} e^{j\delta_m} e^{j\mathbf{r}_m \cdot \mathbf{u}} \quad (3.3)$ This Would Be The Same As The Array Pattern If The Array Consisted Of Ideal Isotropic

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AN-1140. Figure 7. Response Of A 3-Microphone Broadside Array With 75 Mm Spacing Between Each Microphone . Spacing Microphones Closer Together In A Broadside Array Raises The Aliasing Frequency, But Reduces The Attenuation At Lower 4th, 2024

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Elements With The Elements Providing Different Response Patterns. The Other Design Utilizes Unequally Spaced Antenna Elements With All The Elements Providing Identical Response Patterns. The Available Performance Of Both Antenna Arrays For Use With A Correlation Direction Finding Algorithm Is Presented. iii. 4th, 2024

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Balanis. Dr. Balanis Let Me Into His Research Group And Gave Me Funding To Research Array Geometry, Which Ultimately Led To The Work Presented Here. His Guidance And Helpfulness Were Paramount In Producing Successful Research; Without This The Work Would Not Have Been Completed Due To My Youthful Impatience And Wavering Trajectory. 3th, 2024

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LTR LIT L L Jj RI HH Hff Fee $\Omega\Psi = =\Omega\Psi \Psi \sum Krkr Rr Rr G G \Omega$ (7) Where GT And GR Are The Patterns Of The Transmit And Receive Antenna Elements, Respectively, And K Is The Unit Wave Vector In The Direction Of The Lth DOD Or DOA. The Location

Vector $\mathbf{r}_T(i)$ Is Measured From The Position Of The Reference Antenna Of The Transmit Array, And Similarly For The Receive Array. Y. . . X D. . . Fig ... 2th, 2024

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