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1,250°C Gas · 7% Performance (thrust/weight) Improvement Expected · Ceramic Turbine Built But Not Tested. M-DOT Micro-turbine Engine Silicon Nitride Inlet Nozzle And Turbine Palm Size Gas Turbine Engine (thrust Type) φ25 Mm Turbine, 400k Rpm All Metal Components Ran A Few Minutes. Turbine Blades Melted! 1998: DARPA - M-Dot 1th, 2024

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Dr. Drosjack Received His B.S. Degree (Mechanical Engineering, 1970) From Carnegie-Mellon University, And His M.S. (1971) And Ph.D. (1974) Degrees (Mechanical Engineering) From The Ohio State University. He Is A Member Of ASME, The Vibration Institute, The Machinery Subcommittee Of The Ethylene Products Committee, Participates In 4th, 2024

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4.2.1 Ideal Centrifugal Flow Machines Simple Analysis Of Centrifugal Pump Or Fan Impeller Dynamics Leads To The Following Theoretical Head Relationship (Potter And Wiggert, 1997):  $H_t = \omega^2 r_2^2 \frac{2}{g} - \omega \cot \beta_2 \frac{2\pi l_2}{g} Q$  (4.1) Where  $\omega$  Is The Angular Velocity Of The Impeller,  $\beta_2$  Is The Exit Blade Angle,  $r_2$  Is The 3th, 2024

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Considered An Axial Machine Thereby Neglecting Centrifugal Compressors/turbines Without Justi Cation. Also, One Might Want To Have A More Precise Relation For Design Purposes. For All These Reasons, A More Formal Derivation Is Necessary. Alexis Giauque (LMFA/ECL) Turbomachinery Aer 2th, 2024

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Also  $D_h = C_p dT = V dp$  And  $P_v = RT$ . Thus,  $P_{out} / P_{in} = T_{out} / T_{in} = C_p R / (C_p R + W_{12} C_p T_{in} / C_p R)$  (10) Using  $C_p$

= 1kj=kg K, T1 = 288K Gives Pout Pin = 2:55 The Device Studi 3th, 2024

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